

## EFFECT OF EXPANSION RATIO ON DEFLECTION OF CASTELLATED BEAM

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**ABSTRACT:** As we know that, though there is no provision for the castellated beam in Indian standard, the use of castellated beam is increased day by day mainly for the industrial buildings because of the advantage of the castellated beam like decrease the weight of the beam cause decrease floor weight. And decrease of floor weight causes decrease in size and weight of the columns and ultimately considerably reduction in cost of the substructures. A study on the effect of the expansion ratio on the deflection of the castellated beam is described in this paper. Finite element method is used using ANSYS 11 to determine the behavior of the castellated beam with change of the expansion ratio. In this paper, the expansion ratio of different values for the ISMB 500 is used for which, the depth is ranging from 700 to 800 with expansion ratio of 1.4 to 1.6. Here two support conditions one is both ends are fixed and other is both ends are pinned are used and various parameters are found out like maximum von mises stresses, deflections, strain etc. Here there is variation have seen in deflection with change in the expansion ratio. With increase in expansion ratio, there is a decrease in deflection up to certain limit and, then there is a increase in deflection. It is obvious that the deflection is inversely proportional to the moment of inertia of the castellated beam about x-x axis. But after certain limit there is a increase in deflection though there is a increase in moment of inertia due to increase in depth of the section by increasing the expansion ratio. It is because of web buckling due to increase in slenderness ratio, there is a possibility for web buckling of the castellated beam. So the main aim of the paper is to find the minimum deflection i.e. optimized section of the beam using change in expansion ratio.

**Key words:** Castellated beam, Expansion ratio

### I. INTRODUCTION

Economy in construction of steel structure cannot obtained by increasing utilization of high strength steel for the construction. Economical construction can be obtained up to certain extent by using modified steel structure design. So the next way is to modification of standard steel section i.e. castellated beam for flexural member.

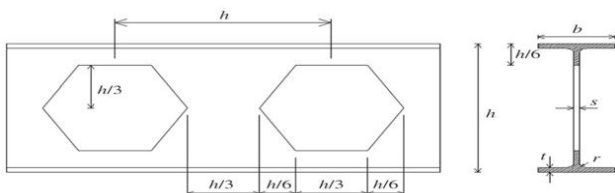


Fig. 1 Castellated beam and opening geometry.

### II. FABRICATION

Profile cutting is done in web of I – section in zigzag manner as shown in fig.2. than these two halves are separated and slid by the length equal to half the width of hollow portion. In this position these two separate parts are joined as shown in fig.2. Remaining portion is considered as a wastage, which is shown by hatch lines as shown in fig.2.

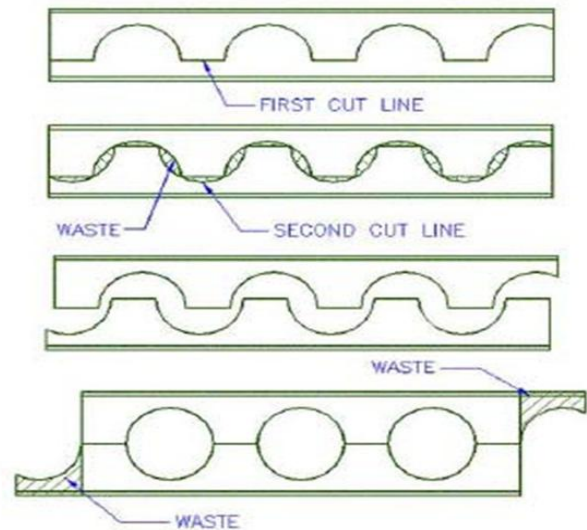


Fig. 2 Fabrication of castellated beam

### III. VIERENDEEL ANALYSIS

A castellated beam having a span of  $L$  and overall depth  $D$  is as shown in fig.3. It is subjected to uniformly distributed load  $q$  Kg/m. For the design of castellated beam it is required to find the maximum stresses in the beam which may occur at any point in the length of the beam within the region of T-section. For convenience of calculation, the beam is analyzed as a vierendeel truss where the longitudinal fiber stress is governed by both the beam bending moment as well as vertical shear. The following assumptions are made in calculating stresses.

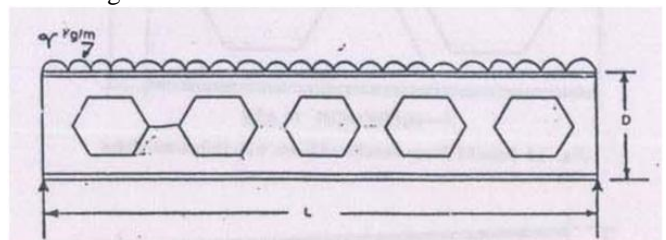


Fig. 3 Typical castellated beam under uniformly distributed superimposed loading.

In the open portion of the web, vertical shear divides equally between the upper and lower tees. For bending moment in the T-section due to shear, point of contraflexure is assumed to exist in the vertical centre line of the open section. Fiber stress varies linearly and the maximum stress in the open section is computed as an algebraic sum of both primary and secondary stresses which are due to shear in the T-section respectively A typical section of a castellated beam is shown in the fig. 4(a) The stress distribution diagram is shown in fig. 4(b).

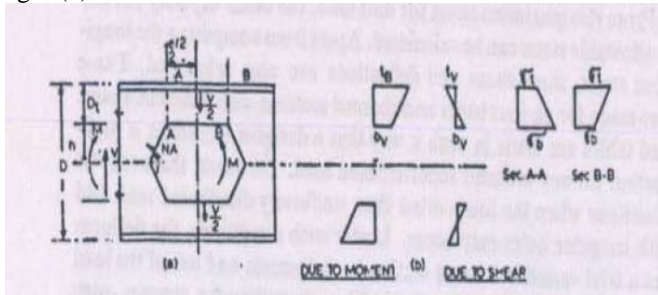


Fig.4 Typical section and distribution of stresses of castellated beam.

Maximum fiber stress at section A-A.

$$\sigma_b = b_B + b_V = \frac{M_A}{I_g} X h + \frac{V \cdot e}{4S_g} \dots \dots \dots (1)$$

Maximum fiber stresses at section B-B.

$$\sigma_t = t_B + t_V = \frac{M_B D}{2I_g} + \frac{V e}{4S_f} \dots \dots \dots (2)$$

The maximum longitudinal fiber stresses can occur at inner edge of the tee web i.e. bending stress at top fiber of the tee i.e. maximum bending stress would occur at section A-A and is computed by the equation 1. The maximum bending stress would occur at section B-B and is computed by equation 2. A castellated beam section is most efficiently used when bending stress at section B-B is governing stress. However, this is not always possible particularly on the short spans.

**Shear Stress analysis**

The shear capacity will be governed by the least area either in the vertical web or in the throat length. Maximum shear stress may generally occur in the throat length except in case where the expansion ratio is high when it may occur in the vertical section. The shear stress in the web elements are calculated as follows. The different forces acting on the element are shown in the fig.5. It is required to find horizontal shear at section X-X which is obtained by taking moment at point C.

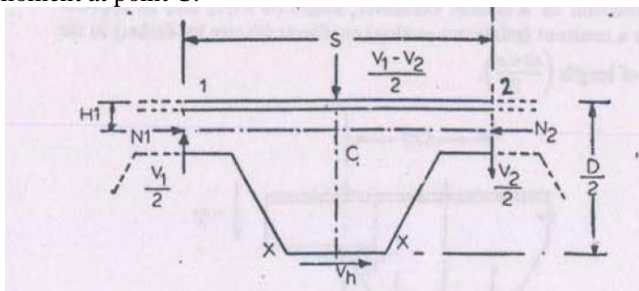


Fig.5 Free body diagram of top segment of the beam.

Free body diagram of top segment of the beam.

$$V_h = \frac{\frac{V_1}{2} X \frac{S}{2} + \frac{V_2}{2} X \frac{S}{2}}{\frac{D}{2} - H_1} = \frac{S}{2} \frac{(V_1 + V_2)}{\frac{D}{2} - H_1}$$

If,

$$V_1 = V_2 = V;$$

$$V_h = \frac{\frac{S}{2} X V}{\frac{D}{2} - H_1};$$

$$V = \frac{2 V_h (\frac{D}{2} - H_1)}{S} \dots \dots \dots (3.3)$$

**IV. RESULT AND DISCUSSIONS**

*Problem & Definition*

Here there is a study of the castellated beam by analyzing the castellated beam with the help of ANSYS WORKBENCH 11. The problem is taken as a 10m span of castellated beam with both end fixed and both and hinged means fixed beam and simply supported beam and fixed beam respectively. The beam is analyzed with 1000pa load on the upper flange of the beam. There is a change in depth of castellated beam from 700 mm to 800 mm with change in expansion ratio from 1.4 to 1.6. The properties of the parent section of the I section is as follow.

- ISMB 500 @ 86.9 Kg/m.
- Sectional area a = 110.74 cm<sup>2</sup>.
- Depth of the beam D = 500 mm.
- Width of the beam B<sub>f</sub> = 180 mm.
- Thickness of the web t<sub>w</sub> = 10.2 mm.
- Thickness of the flange t<sub>f</sub> = 17.2 mm.
- Slope of flange = 98°.
- Radius at root Y<sub>1</sub> = 17.0 mm.
- Radius at toe Y<sub>2</sub> = 8.5 mm.
- Moment of inertia I<sub>xx</sub> = 45218.3 cm<sup>4</sup>.
- Moment of inertia I<sub>yy</sub> = 1369.8 cm<sup>4</sup>
- Radius of gyration r<sub>xx</sub> = 20.21 cm.
- Radius of gyration r<sub>yy</sub> = 3.52 cm.
- Section modulus Z<sub>xx</sub> = 1808.7 cm<sup>3</sup>.
- Section modulus Z<sub>yy</sub> = 152.2 cm<sup>3</sup>.

The results obtained are as follows.

- Deflection of the castellated beam for the fixed beam as well as simply supported beam for each expansion ratio.
- Maximum von mises stresses for each expansion ratio of the castellated beam for fixed as well as simply supported beam.
- Maximum strain for each expansion ratio for the fixed beam as well as simply supported beam.
- The above results are used to generates,
- The relationship between the deflection v/s depth of the castellated beam means depth of the hole.
- The relationship between the deflection v/s Expansion ratio of the castellated beam
- The relationship between the maximum von mises stresses v/s depth of the castellated beam.
- The relationship between the maximum von mises stresses v/s expansion ratio of the castellated beam.
- The relationship between the maximum deflection v/s angle of inclination of the castellated beam.

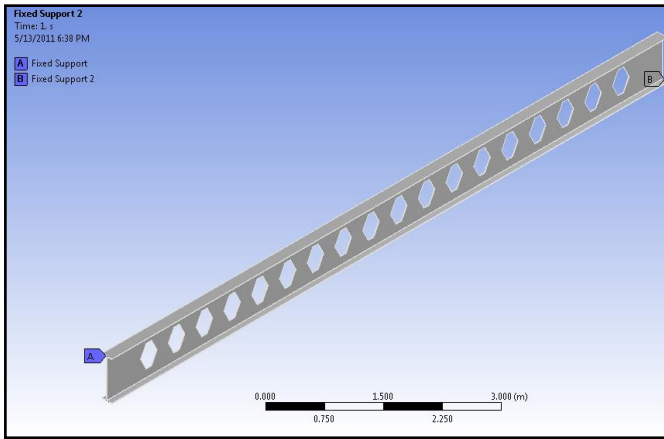


Fig.6 Figure showing the castellated beam analyzed in ANSYS

**Results & Discussion**

From the problem of castellated beam, the castellated beam is analyzed with same loading with uniformly distributed load of 1000 pa. And the expansion ratio is vary from 1.4 to 1.6 and the depth of castellated beam of parent section ISMB 500 is varying from 700 mm to 800 mm with 2 mm increment with 50 nos. of models.

For this castellated beam, the castellated beam is analyzed and the parameters obtained are as follows.

- The maximum deflection of the beam.
- The maximum von mises stresses in the beam.
- The maximum strain in the beam.

- From the above results, the following graphs are plotted
- Deflection v/s depth of the castellated beam.
- Deflection v/s angle of inclination.
- Deflection v/s expansion ratio.
- Max. stress v/s depth of castellated beam.
- Max. stress v/s expansion ratio.

Table 1 Analysis Results For Fixed beam

Dep th	Expans ion ratio	DEFLECT ION (mt.)	Angle of inclinatio n $\theta^\circ$	Max Stress (N/m2 )	Max Strain
700	1.4	2.90E-02	89.84924 432	29030 00	0.0038 215
702	1.404	2.89E-02	89.84924 432	28880 00	0.0039 1
704	1.408	2.88E-02	89.84924 432	28750 00	0.0038 95
706	1.412	2.85E-02	89.84924 432	28490 00	0.0039 38
708	1.416	2.85E-02	89.84924 432	28530 00	0.0039 22
710	1.42	2.85E-02	89.84924 432	28500 00	0.0039 15
712	1.424	2.85E-02	89.84924 432	28480 00	0.0039 04
714	1.428	2.82E-02	89.84924 432	28200 00	0.0037 8

716	1.432	2.85E-02	89.84924 432	28450 00	0.0039 78
718	1.436	2.83E-02	89.84924 432	28340 00	0.0040 4
720	1.44	2.83E-02	89.84924 432	28250 00	0.0034 77
722	1.444	2.79E-02	89.84924 432	27920 00	0.0040 17
724	1.448	2.78E-02	89.84924 432	27760 00	0.0033 52
726	1.452	2.81E-02	89.84924 432	28120 00	0.0036 1
728	1.456	2.77E-02	89.84924 432	27740 00	0.0039 96
730	1.46	2.83E-02	89.84924 432	28300 00	0.0035 79
732	1.464	2.76E-02	89.84924 432	27570 00	0.0044 43
734	1.468	2.77E-02	89.84924 432	27740 00	0.0036 82
736	1.472	2.76E-02	89.84924 432	27580 00	0.0037 38
738	1.476	2.70E-02	89.84924 432	26960 00	0.0037 2
740	1.48	2.76E-02	89.84924 432	27610 00	0.0039 33
742	1.484	2.74E-02	89.84924 432	27400 00	0.0043 07
744	1.488	2.73E-02	89.84924 432	27310 00	0.0036 81
746	1.492	2.68E-02	89.84924 432	26770 00	0.0038 1
748	1.496	2.67E-02	89.84924 432	26680 00	0.0037 42
750	1.5	2.64E-02	89.84924 432	26370 00	0.0039 22
752	1.504	2.73E-02	89.84924 432	27330 00	0.0039 68
754	1.508	2.71E-02	89.84924 432	27060 00	0.0037 7
756	1.512	2.69E-02	89.84924 432	26930 00	0.0044 1
758	1.516	2.65E-02	89.84924 432	26490 00	0.0044 51
760	1.52	2.64E-02	89.84924 432	26425 00	0.0043 744
762	1.524	2.65E-02	89.84924 432	26520 00	0.0044 183
764	1.528	2.63E-02	89.84924 432	26310 00	0.0036 63
766	1.532	2.61E-02	89.84924 432	26090 00	0.0042 71
768	1.536	2.66E-02	89.84924 432	26580 00	0.0042 51
770	1.54	2.66E-02	89.84924 432	26630 00	0.0041 313

772	1.544	2.68E-02	89.84924 432	26830 00	0.0047 596
774	1.548	2.73E-02	89.84924 432	27270 00	0.0042 05
776	1.552	2.69E-02	89.84924 432	26920 00	0.0046 999
778	1.556	2.66E-02	89.84924 432	26630 00	0.0041 142
780	1.56	2.67E-02	89.84924 432	26657 00	0.0043 29
782	1.564	2.61E-02	89.84924 432	26060 00	0.0044 138
784	1.568	2.61E-02	89.84924 432	26070 00	0.0043 89
786	1.572	2.60E-02	89.84924 432	26000 00	0.0049 99
Dep th	Expans ion ratio	DEFLECT ION (mt.)	Angle of inclinatio n $\theta^\circ$	Max Stress (N/m2 )	Max Strain
788	1.576	2.60E-02	89.84924 432	25970 00	0.0041 53
790	1.58	2.60E-02	89.84924 432	25980 00	0.0045 37
792	1.584	2.61E-02	89.84924 432	26050 00	0.0045 416
794	1.588	2.59E-02	89.84924 432	25870 00	0.0047 29
796	1.592	2.59E-02	89.84924 432	25910 00	0.0045 18
798	1.596	2.67E-02	89.84924 432	26730 00	0.0059 29
800	1.6	2.67E-02	89.84924 432	26682 00	0.0061 45

Table 2 Analysis Results For Simply supported beam

DE PT H	Expan sion ratio	DEFLE CTION (mt.)	Angle of inclinat ion $\theta^\circ$	Max stress (N/mm2 )	Ma x. stra in
700	1.400	0.0289	8.0686	8.25570 E+06	0.0 041 0
702	1.404	0.0282	8.2979	8.22040 E+06	0.0 041 1
704	1.408	0.0299	8.1397	8.56710 E+06	0.0 042 8
706	1.412	0.0299	7.4271	7.79510 E+06	0.0 039 0
708	1.416	0.0303	7.2068	7.66690 E+06	0.0 038 3
710	1.420	0.0282	8.2782	8.21730 E+06	0.0 041 1

712	1.424	0.0296	8.1699	8.50770 E+06	0.0 042 5
714	1.428	0.0298	8.7681	9.18380 E+06	0.0 045 9
716	1.432	0.0297	7.9240	8.26010 E+06	0.0 041 3
718	1.436	0.0292	8.8980	9.14980 E+06	0.0 045 8
720	1.440	0.0292	9.3287	9.59350 E+06	0.0 048 0
722	1.444	0.0293	7.9126	8.13360 E+06	0.0 040 7
724	1.448	0.0290	8.3842	8.54040 E+06	0.0 042 7
726	1.452	0.0290	8.9157	9.08930 E+06	0.0 045 5
728	1.456	0.0289	8.9403	9.08440 E+06	0.0 045 4
730	1.460	0.0288	7.8764	7.98010 E+06	0.0 039 9
732	1.464	0.0238	10.491 0	8.81750 E+06	0.0 044 1
734	1.468	0.0272	8.1985	7.83770 E+06	0.0 039 2
736	1.472	0.0271	9.0672	8.65080 E+06	0.0 043 3
738	1.476	0.0269	8.3480	7.89210 E+06	0.0 039 5
740	1.480	0.0269	8.5481	8.12700 E+06	0.0 040 5
742	1.484	0.0268	8.5597	8.07970 E+06	0.0 040 4
744	1.488	0.0268	8.9154	8.39560 E+06	0.0 042 0
746	1.492	0.0266	8.5358	7.98180 E+06	0.0 039 9
748	1.496	0.0266	7.5764	7.07110 E+06	0.0 035 4

750	1.500	0.0263	9.2911	8.61150 E+06	0.0 043 1
752	1.504	0.0266	8.0277	7.49160 E+06	0.0 037 5
754	1.508	0.0264	7.6996	7.13570 E+06	0.0 035 7
DE PT H	Expan sion ratio	DEFLE CTION (mt.)	Angle of inclinat ion $\theta^\circ$	Max Stress (N/m <sup>2</sup> )	Ma x. stra in
756	1.512	0.0263	8.3364	7.76220 E+06	0.0 038 5
758	1.516	0.0261	7.9280	7.26330 E+06	0.0 036 3
760	1.520	0.0260	9.0920	8.32500 E+06	0.0 041 6
762	1.524	0.0260	9.3691	8.56890 E+06	0.0 042 9
764	1.528	0.0259	9.3866	8.55030 E+06	0.0 042 8
766	1.532	0.0258	9.2224	8.38880 E+06	0.0 041 9
768	1.536	0.0278	7.7793	7.58720 E+06	0.0 037 9
770	1.540	0.0277	7.7678	7.55210 E+06	0.0 037 8
772	1.544	0.0275	7.3665	6.91640 E+06	0.0 035 6
774	1.548	0.0275	8.0522	7.78350 E+06	0.0 038 9
776	1.552	0.0270	7.7719	7.38460 E+06	0.0 036 9
778	1.556	0.0256	9.2882	8.21020 E+06	0.0 042 0
780	1.560	0.0256	8.5492	7.71160 E+06	0.0 038 6
782	1.564	0.0255	8.2324	7.36100 E+06	0.0 036 9
784	1.568	0.0255	8.6428	7.74010 E+06	0.0 038

					7
786	1.572	0.0253	8.6334	7.69720 E+06	0.0 038 5
788	1.576	0.0253	9.2956	8.28200 E+06	0.0 041 4
790	1.580	0.0252	8.2142	7.29060 E+06	0.0 036 5
792	1.584	0.0366	6.0063	7.14800 E+06	0.0 038 6
794	1.588	0.0251	8.3646	7.39560 E+06	0.0 037 0
796	1.592	0.0251	9.1568	8.10110 E+06	0.0 040 5
798	1.596	0.0255	7.0070	6.26360 E+06	0.0 031 3
800	1.600	0.0255	7.6264	6.82080 E+06	0.0 034 1

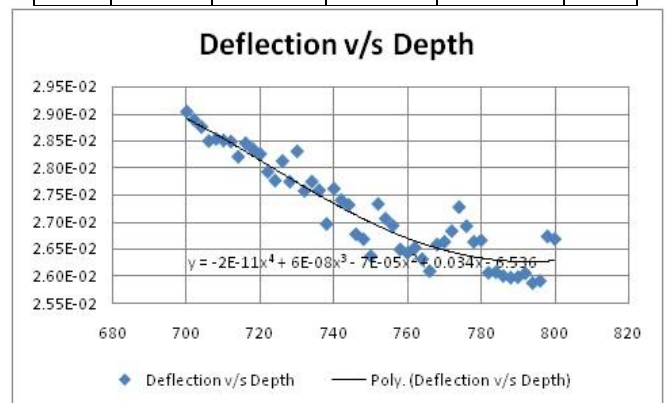


Fig. 7 Deflection v/s Depth of the castellated beam for fixed beam

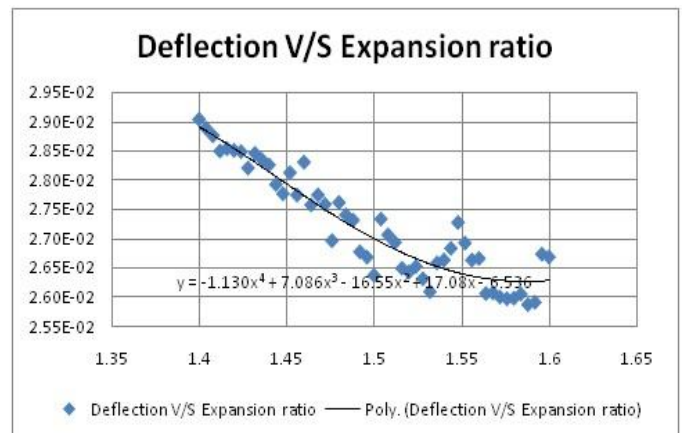


Fig. 8 Deflection V/S Expansion ratio of castellated beam for fixed beam

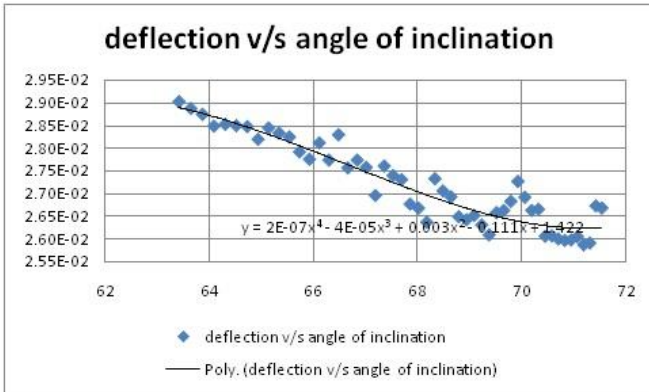


Fig.9 Deflection V/S Angle of inclination of castellated beam for fixed beam

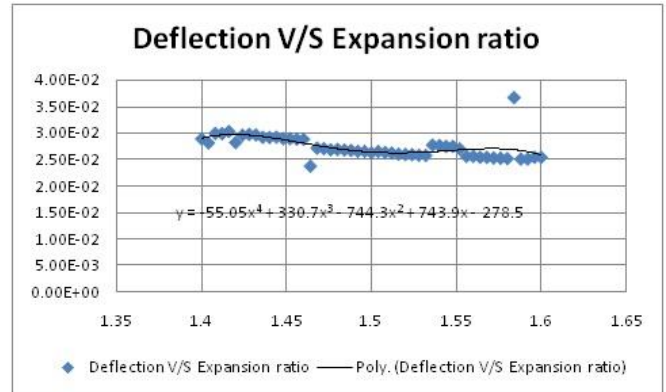


Fig.13 Deflection V/S Expansion ratio of the castellated beam for the simply supported beam

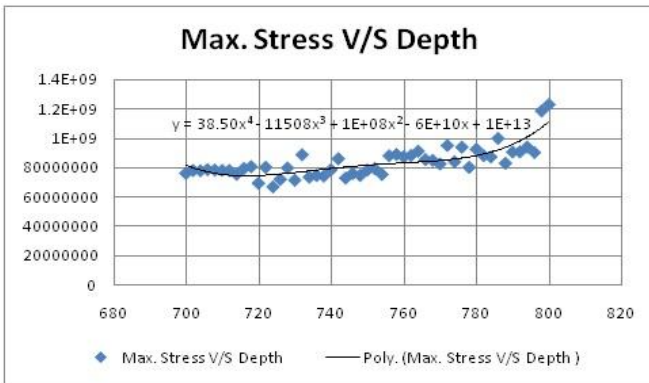


Fig.10 Maximum stress V/S Depth of castellated beam for fixed beam

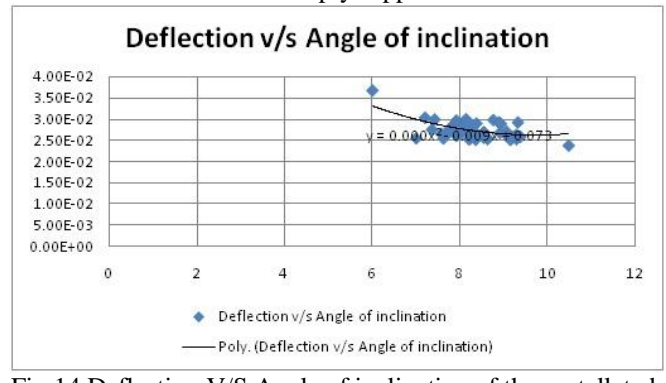


Fig.14 Deflection V/S Angle of inclination of the castellated beam for the simply supported beam

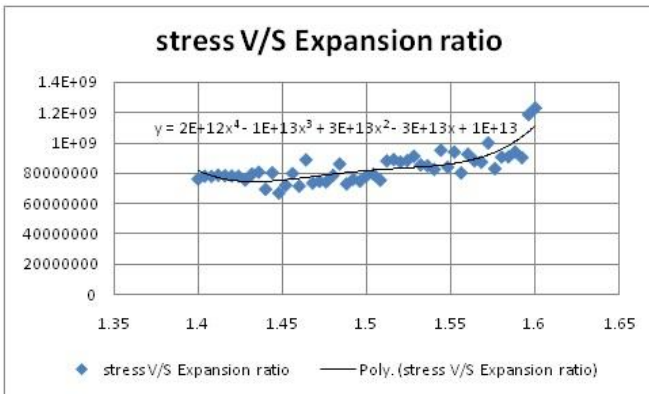


Fig.11 Maximum stress V/S Expansion ratio of castellated beam for fixed beam

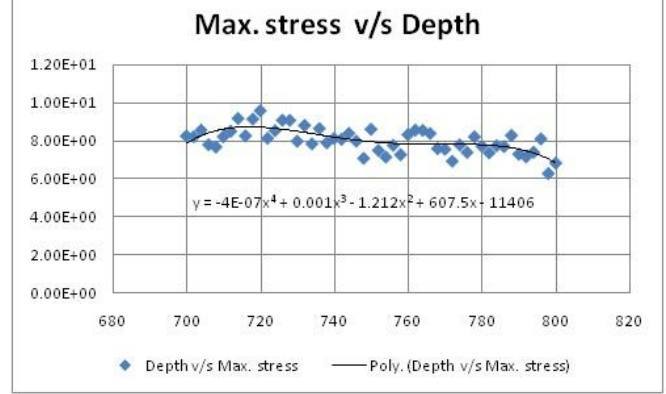


Fig.15 Max. stress V/S Depth of the castellated beam for the simply supported beam

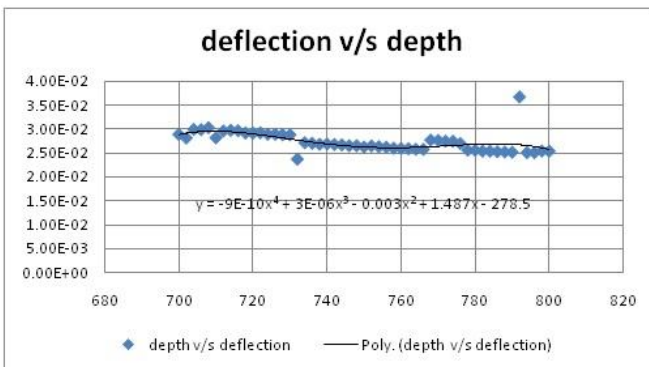


Fig.12 Deflection V/S Depth of the castellated beam for the simply supported beam

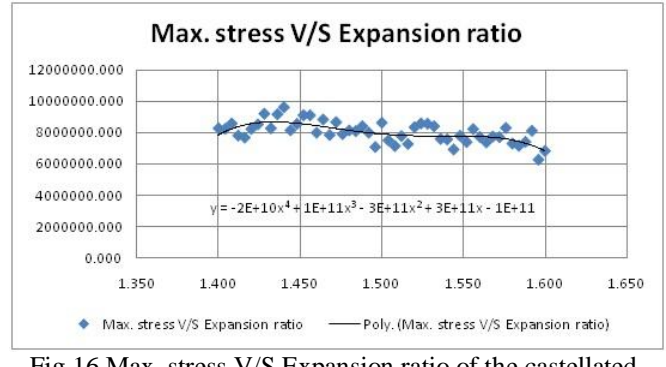


Fig.16 Max. stress V/S Expansion ratio of the castellated beam for the simply supported beam

V. CONCLUSION

The main objective of this thesis is to know the behavior of the castellated beam under static gravity loading, as well as to calculate the minimum deflection of the castellated beam corresponding to expansion ratio, depth as well as the angle of inclination. The following results have been obtained for the castellated beam under static gravity loading for the different and condition. First is the ends have restrained against vertical as well as horizontal displacements only. Second is restrained against the vertical, horizontal as well as rotational.

Table 3 Analysis result summary for Fixed beam

	Deflection (m)	Max. stress (N/m <sup>2</sup> )	Max. strain
Minimum	2.5870E-02	2587000.0000	0.0034
Depth	7.8800E+02	788.0000	724.0000
Expansion ratio	1.5760E+00	1.5760	1.4480
Angle of inclination	7.0823E+01	70.8234	65.9161

Table 4 Analysis result summary for Simply supported beam

	Deflection(m)	Max. stress(N/m <sup>2</sup> )	Max. strain
Minimum	2.38000E-02	6263600.0000	0.00313
Depth	732	798.00000	724
Expansion ratio	1.464	1.59600	1.448
Angle of inclination	66.6555	70.82336	71.4210

From the results, it is observed that, for the fixed end beam and simply supported beam, the minimum deflection, Max. von misses stresses and the Max. strain values of the parameters like angle of inclination, depth and expansion ratios are different. So to reduce the stress, strain or deflection, it is obvious to adopt the particular parameters like angle of inclination, depth and expansion ratio.

- As it is observed from the deflection vs depth curve that the deflection is gradually decreasing with increase in depth but after some value of depth it remains constant for a particular intensity of load.
- The similar trends can be observed from the curves of deflection vs expansion ratio, and deflection vs angle of inclination.
- It is observed that stress value attains higher magnitude with higher values of depth of the beam.
- The similar trend can be observed from the curve of stress vs expansion ratio, and stress vs angle of inclination.
- Defferent boundary conditions affect the deformation parameters of the beam.

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Software

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