

SQUEEZE FILM IN SPHERICAL BEARING WITH TWO LAYER FLUID CONSIDERING THERMAL EFFECT AND VISCOSITY VARIATION

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ABSTRACT: In this paper the squeeze film lubrication of spherical bearing considering viscosity variation and thermal effects are analyzed. Expressions for load capacity and squeezing time are obtained and analyzed numerically, graphs are plotted. It is shown that the load capacity and time of squeezing increases due to high viscous layer near the periphery and decreases due to low viscous layer. A parameter 'q' is introduced to see the thermal effect in load capacity and squeezing time for spherical bearing and analyzed for different parameters.

Key Words: squeeze film, viscosity, eccentricity, thermal effect, film thickness, squeezing time etc.,

I. INTRODUCTION

The phenomenon of two lubricated surfaces approaching each other with a normal velocity is known as squeeze film lubrication. The thin film of lubricant present between the two surfaces acts as a cushion and it prevents the surfaces from making instantaneous contact. The time required to squeeze out the lubricant depends upon surface configuration, fluid properties and the load applied. In general, the relation between the load carrying capacity and the rate of approach is studied in the most squeeze film analysis. Much work is done in this line and the mathematical review on such process was done by various workers [1-47]. Although squeeze film lubrication has been generally understood for sometimes, the importance of applications lead to draw the attention of many workers in sixties. Pan et.al [30] studied the theory and experiments of squeeze film bearing parti-cylindrical journal bearings. Jacson.J.D [20]studied a study of squeezing flow. Gould.P [14] studied about parallel surface squeeze films: The effects of variation of viscosity with temperature and pressure. Beck et.al [4] studied flat disk squeeze film bearing including the effects of supported mass motion. Ramaiah.G and Dubey J.N [34] studied squeeze films and thrust bearing using Micro polar fluid. Murti.P.R.K [26] studied squeeze films in porous bearings. J.B.Shukla, K.R.Prasad and P.Chandra studied various squeeze films using power law fluid [21]. In this paper the squeeze film lubrication of spherical bearing considering viscosity variation and thermal effects are analyzed. Expressions for load capacity and squeezing time are obtained and analyzed numerically, graphs are plotted. A parameter 'q' is introduced to see the thermal effect in load capacity and squeezing time for analyzing due to it.

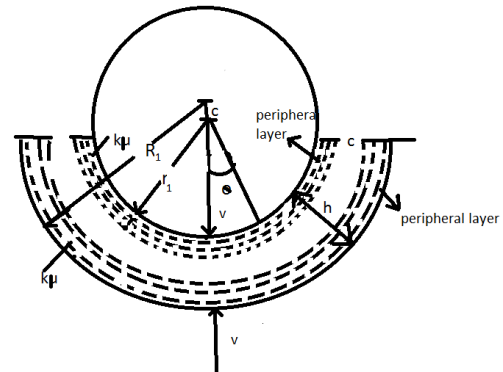


Fig (1.1): SQUEEZE FILM IN SPHERICAL BEARING

II. SQUEEZE FILM LUBRICATION IN SPHERICAL BEARING

Consider squeezing between two eccentric spherical surfaces of radii r_1 and R_1 which are approaching each other with a normal velocity V as shown in Fig (1.1).

The film thickness h is given by $h = c(1 - \epsilon \cos \theta)$. Where $c = R_1 - r_1$ is the clearance width and $\epsilon = e/c$ is the eccentricity ratio.

The flow flux in this case is obtained by

$$Q = \left[\frac{F}{r} \frac{dp}{d\theta} 2\pi r_1 \sin \theta \right] \quad (1.1)$$

the flux Q obtained from the equation of continuity is

$$Q = 2\pi r_1 V \sin^2 \theta \quad (1.2)$$

Where

$$F = \frac{1}{12\mu} \frac{\left(1 - \frac{a}{h}\right)^3 (k-1) + 1}{k} \quad (1.3)$$

$$\text{From (1.1) and (1.2) } \frac{dp}{d\theta} = \frac{r_1 V \sin \theta}{F} \quad (1.4)$$

Integrating (1.4) equation using the boundary condition

$p = 0$ at $\theta = \frac{\pi}{2}$ We get the expression for pressure distribution as

$$p(\theta) = \int_0^\theta \left[\frac{r_1 V \sin \theta}{F} \right] d\theta \quad (1.5)$$

If
$$\mu = \mu_0 \left(\frac{h}{h_0}\right)^q$$
 (1.6)

Then
$$F = \frac{1}{12\mu_0 \left(\frac{h}{h_0}\right)^q} \frac{[(1-\frac{a}{h})^3(k-1)+1]}{k}$$
 (1.7)

The load capacity W is given by

$$W = 2\pi r_1^2 \int_0^{\pi/2} p \sin \theta \cos \theta d\theta$$
 (1.8)

Using (1.5) in (1.7) we get the load capacity W as

$$W = 2\pi r_1^3 V \int_0^{\pi/2} \left[\frac{\sin^2 \theta \cos \theta}{F} \right] d\theta$$
 (1.9)

Where
$$F = \frac{h_0^q h^{-q} [(1-\frac{a}{h})^3(k-1)+1]}{12\mu_0 k}$$
 (1.10)

And squeeze time \bar{t} for the surfaces to approach from the initial eccentric position ($\varepsilon=0$) to a final eccentric position ($\varepsilon = \varepsilon_1$) we get

$$\bar{t} = \int_0^{\varepsilon_1} I_1 d\varepsilon$$
 (1.11)

Where
$$I_1 = \int_0^{\pi/2} \left[\frac{\sin^2 \theta \cos \theta}{F} \right] d\theta$$

The graphs are plotted for equations (1.9) and (1.11) are analyzed numerically.

III. RESULTS AND DISCUSSION

Figures (1.2) to (1.7) are drawn for load capacity and squeezing time are plotted with a, q for various parameters ε, k and a .

Fig (1.2) is plotted for load capacity with 'a' for different 'k'. From this figure we can say with the increase of 'k' the load capacity increases and load capacity decreases with decrease of 'k' for increasing 'a'

Fig (1.3) is plotted for load capacity with 'q' for different 'ε'. From this figure we can say with the increase of 'q' the load capacity decreases for increasing of eccentricity 'ε'

Fig (1.4) is plotted for load capacity with 'q' for different k. From this figure we can say with the increase of 'q' the load capacity decreases for decreasing values of 'k'.

Fig (1.5) is plotted for load capacity with 'q' for different 'a'. From this figure we can say with the increase of 'q' the load capacity decreases for decreasing values of 'a'.

Fig (1.6) is plotted for squeezing time with 'a' for different 'k'. From this figure we can say the squeezing time decreases for decreasing 'k' and squeezing time increases for increasing 'k' for increasing values of a

Fig (1.7) is plotted for squeezing time with 'q' for different 'k'. From this figure we can say with the increase of 'q' the squeezing time decreases for decreasing 'k'.

IV. GRAPHS

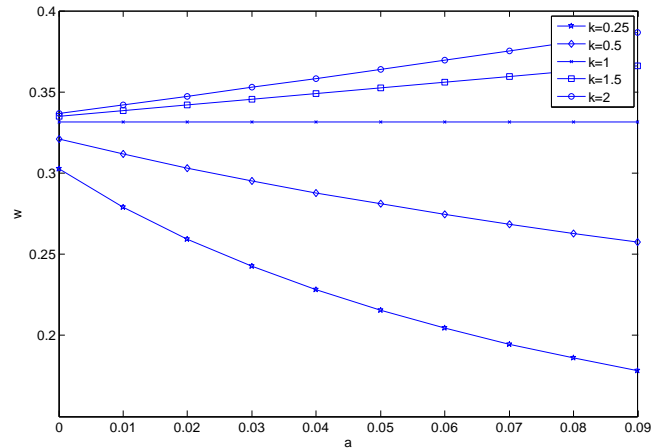


Fig (1.2): Load carrying capacity Vs a for various k, $\varepsilon=0.1, q=0.1$

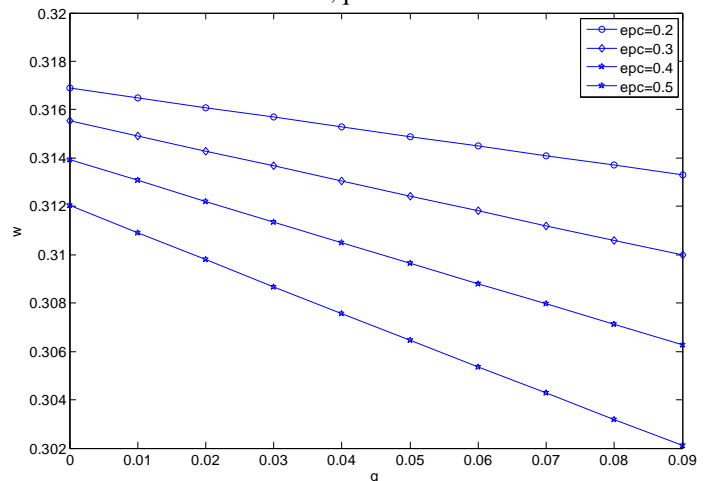


Fig (1.3): Load carrying capacity Vs q for various ε, at k=0.4 and a=0.01

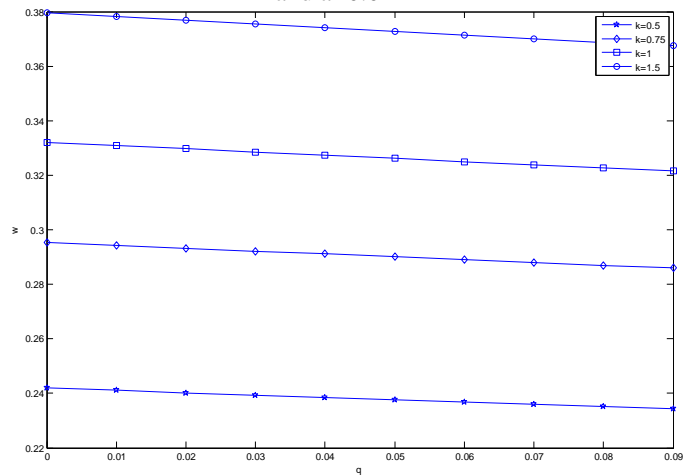


Fig (1.4): Load carrying capacity Vs q for various k, a=0.01 and ε=0.5

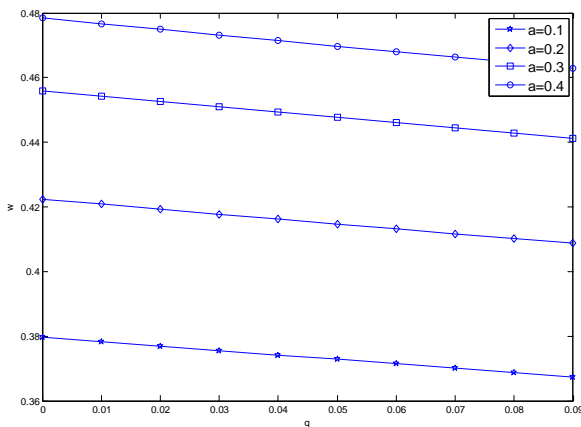


Fig (1.5): Load carrying capacity Vs q for various a, k=1.5 and ε=0.5

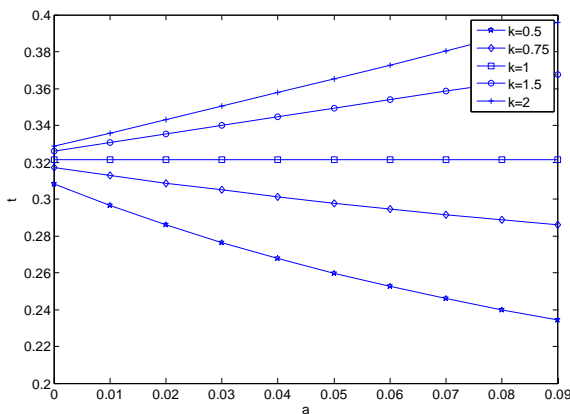


Fig (1.6): Squeezing time Vs a for various k, ε=0.2 to 0.3 and q=0.1

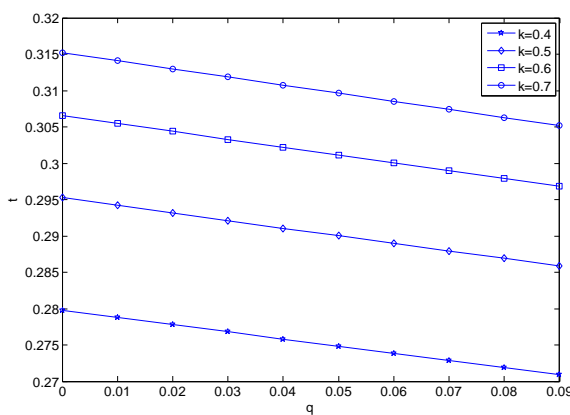


Fig (1.7): Squeezing time Vs q for various k, a=0.03 and ε=0.2 to 0.3

V. SUMMARY

It is observed that the load capacity increases for increasing values of k, a and the squeezing time is also increases for increasing values of k, a but when thermal factor increases the load capacity decreases. It is shown that the load capacity and time of squeezing increases due to high viscous layer near the periphery layer and decreases due to low viscous

layer. It is also observed that the load capacity decreases as thermal factor increases for different parameters.

NOMENCLATURE

- c Clearance width in journal bearing or spherical bearing
- h Film thickness of hydrodynamic Zone
- k Ratio of viscosities in different layers
- p Hydrodynamic pressure
- r₁ Radius of the journal or the radius of the spheres
- R₁ Radius of the bearing
- V Squeeze velocity
- W Load capacity for stiff surfaces
- X Cartesian coordinate in the direction of flow
- μ Viscosity of the purely hydrodynamic zone
- ε Eccentricity ratio
- q Thermal factor
- a peripheral layer thickness

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